

Inference about the plastic behavior of materials from experimental data

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Conference on Sensitivity Analysis of Model Output

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Overview

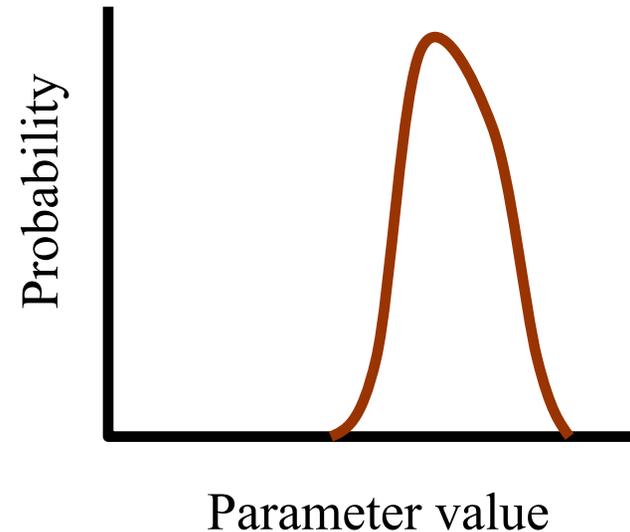
- Understanding physics simulations codes
 - ▶ employ hierarchy of experiments, from basic to fully integrated
 - ▶ role of Bayesian analysis - improve knowledge of models with each new experiment
- Analysis of experimental data to infer parameters of Preston-Tonks-Wallace plasticity model for tantalum
 - ▶ characterize uncertainties in measurement data
 - ▶ estimate PTW parameters and their uncertainties
 - ▶ demonstrate importance of including correlations

Bayesian analysis in context of physics simulations

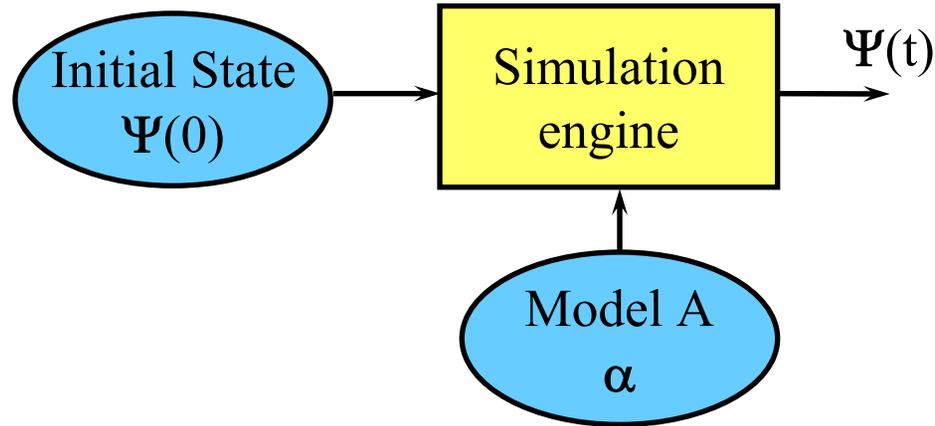
- Goal - describe uncertainties in simulations
 - ▶ physics submodels
 - ▶ experimental (set up and boundary) conditions
 - ▶ calculations (grid size, ...)
- Use best knowledge of physics processes
 - ▶ rely on expertise of physics modelers and experimental data
- Bayesian foundation
 - ▶ focus is as much on uncertainties in parameters as on their best value
 - ▶ use of prior knowledge, e.g., previous experiments and expert judgement
 - ▶ model checking; does model agree with experimental data?

Bayesian uncertainty analysis

- Uncertainties in parameters are characterized by probability density functions (pdf)
- Probability interpreted as quantitative measure of “**degree of belief**”
- This interpretation sometimes called “subjective probability”
- Rules of classical probability theory apply

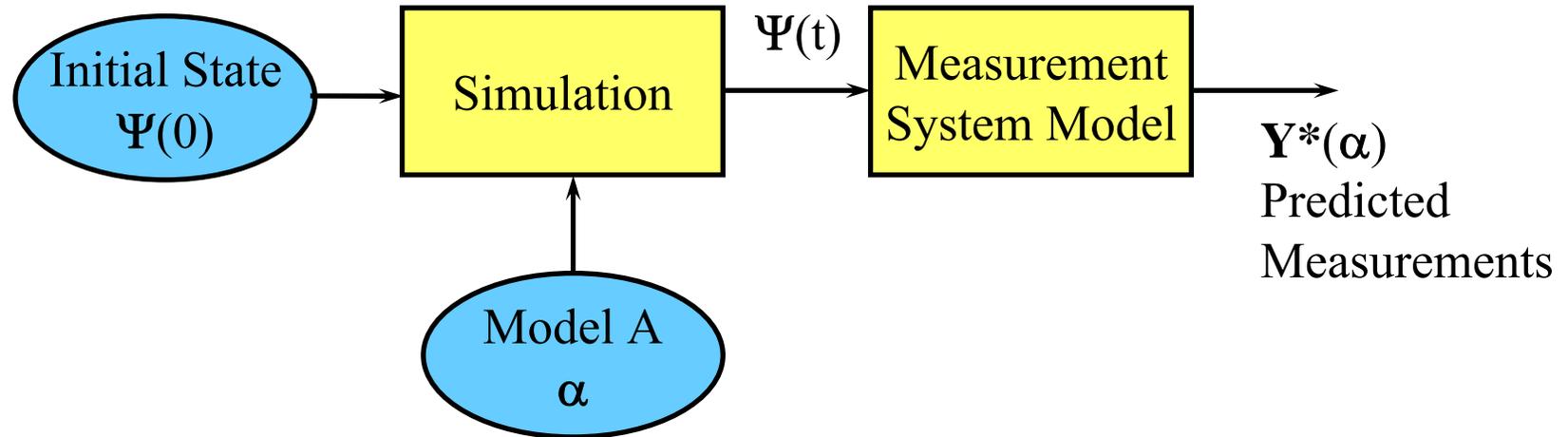


Schematic view of simulation code



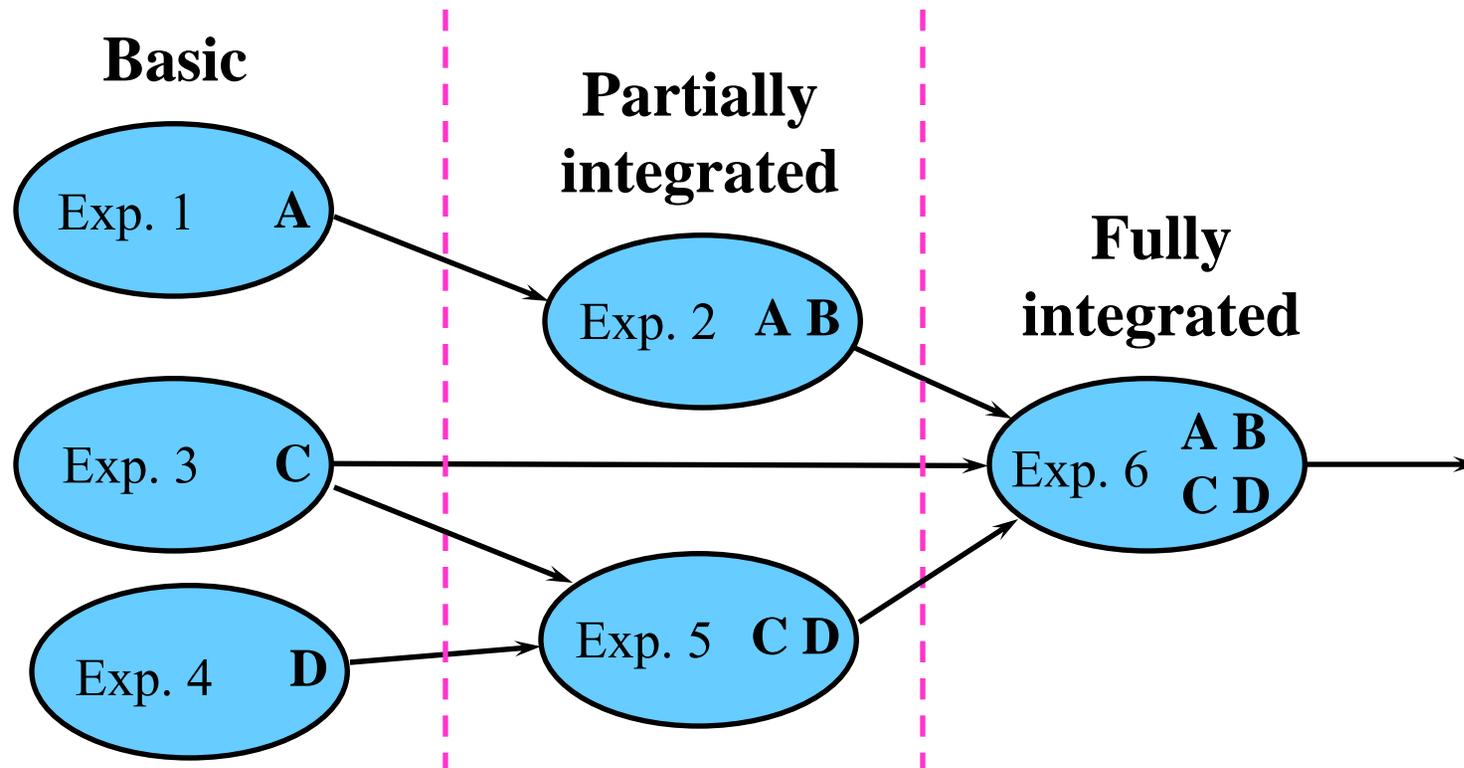
- Simulation code predicts state of time-evolving system $\Psi(t)$
- Requires as input
 - ▶ $\Psi(0)$ = initial state of system
 - ▶ description of physics behavior of each system component; e.g., physics model A with parameter vector α (e.g., constitutive relations)
- Simulation engine solves the dynamical equations (PDEs)
- Uncertainty in $\Psi(t)$ derive from uncertainties in $\Psi(0)$, A, α , and calculational errors

Simulation code predicts measurements



- Simulation code predicts state of time-evolving system
 $\Psi(t)$ = time-dependent state of system
- Model of measurement system yields predicted measurements
- Measurements provide insight about simulation models
- Comparison of experimental to predicted measurements forms basis for inference about simulation code and submodels

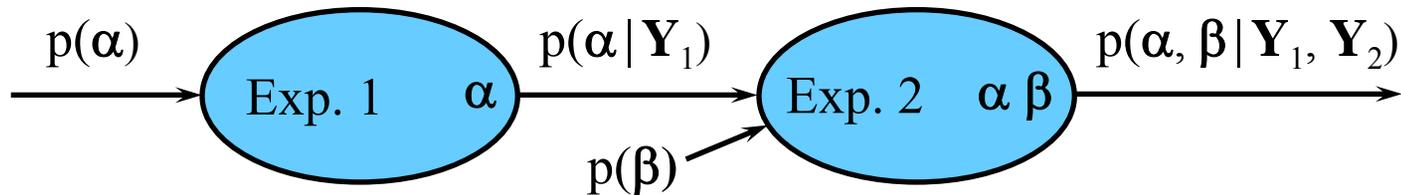
Analysis of hierarchy of experiments



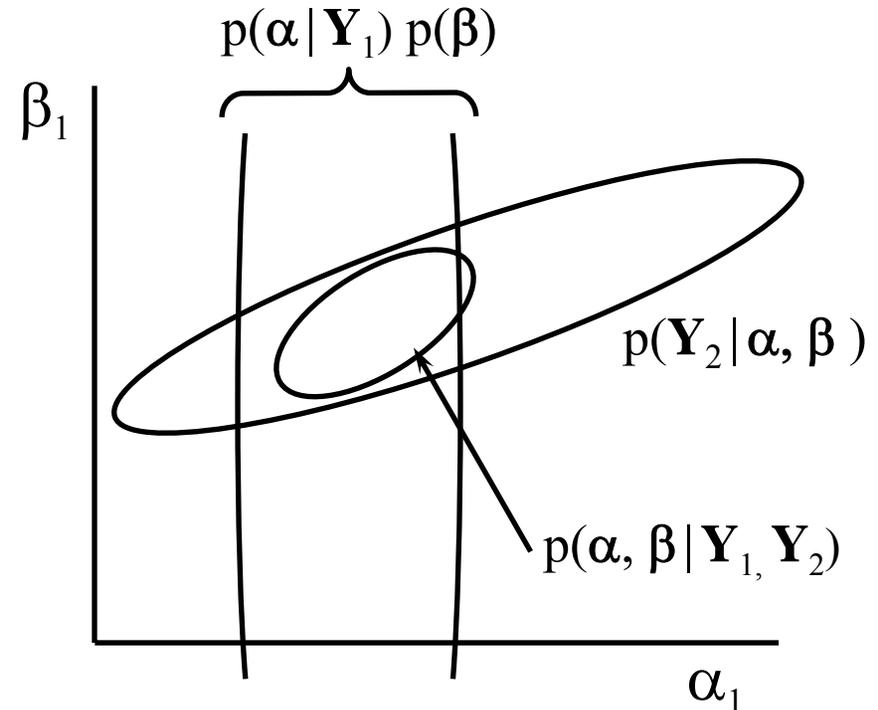
- Information flow in analysis of series of experiments
- Bayesian calibration –
 - ▶ analysis of each experiment updates model parameters (represented as A, B, C, etc.) and their uncertainties, consistent with previous analyses
 - ▶ information about models accumulates

Graphical probabilistic modeling

Propagate uncertainty through analyses of two experiments



- First experiment determines α , with uncertainties given by $p(\alpha | \mathbf{Y}_1)$
- Second experiment not only determines β but also refines knowledge of α
- Outcome is joint pdf in α and β , $p(\alpha, \beta | \mathbf{Y}_1, \mathbf{Y}_2)$ (correlations important!)

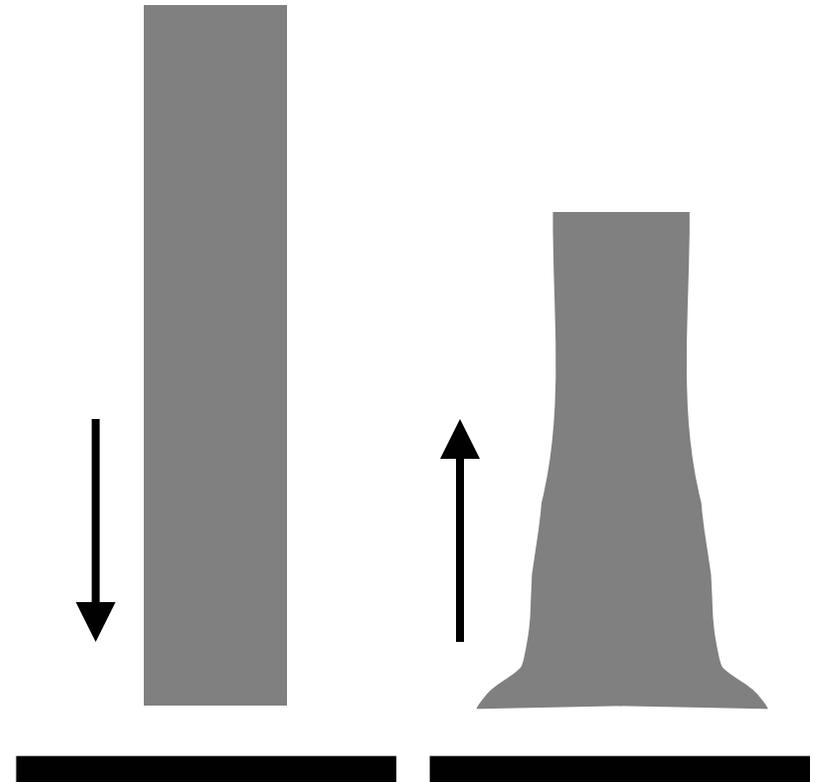


Uncertainty quantification for simulation codes

- Goal is to develop an uncertainty model for the simulation code by comparison to experimental measurements
 - ▶ determine and quantify sources of uncertainty
 - ▶ uncover potential inconsistencies of submodels with expts.
 - ▶ possibly introduce additional submodels, as required
- Recursive process
 - ▶ aim is to develop submodels that are consistent with all experiments (within uncertainties)
 - ▶ a hierarchy of experiments helps substantiate submodels over wide range of physical conditions
 - ▶ each experiment potentially advances our understanding

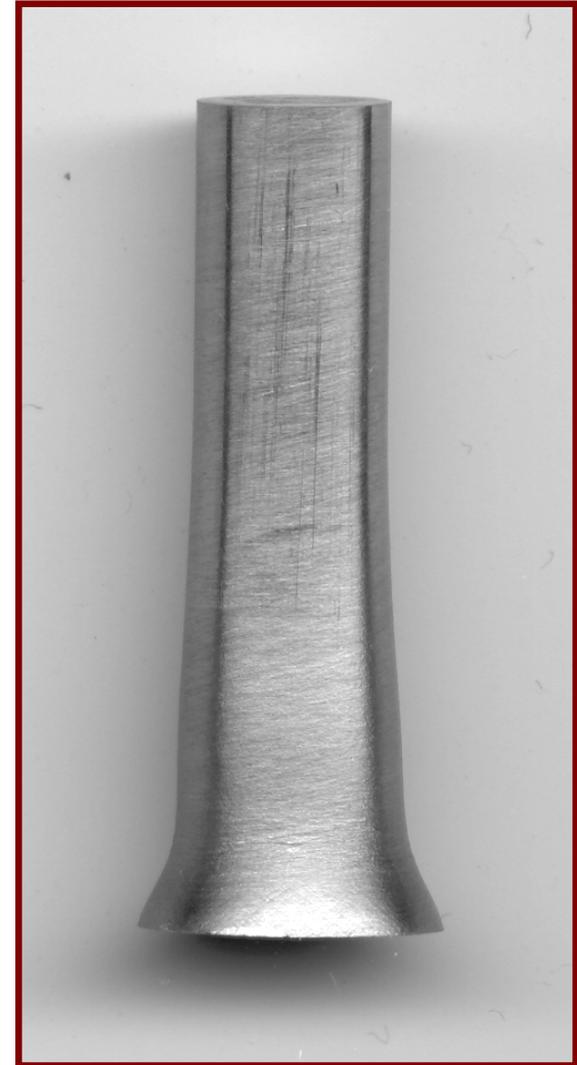
Taylor impact test

- Propel cylinder into rigid plate
- Measure profile of deformed cylinder
- Deformation depends on
 - ▶ cylinder dimensions
 - ▶ impact velocity
 - ▶ plastic flow behavior of material at high strain rate
- Useful for
 - ▶ validating simulation code (including material model)
 - ▶ improving knowledge of parameters in material-behavior model



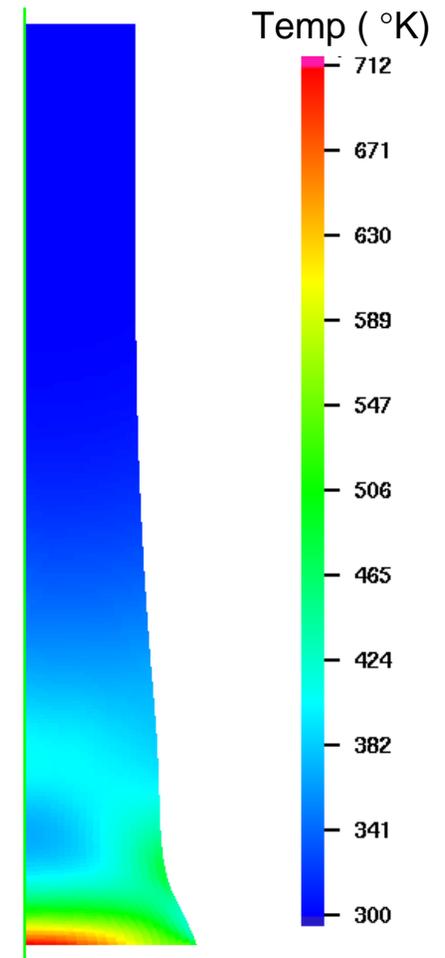
Taylor impact test experiment

- Taylor impact test specimen
 - ▶ high-strength steel, HSLA 100
 - ▶ room temperature, 298 °K
 - ▶ impact velocity = 245.7 m/s
 - ▶ dimensions, final/initial
 - length 31.84 mm / 38 mm
 - diameter 12.00 mm / 7.59 mm
 - ▶ experiment performed by MST-8



Taylor test simulations

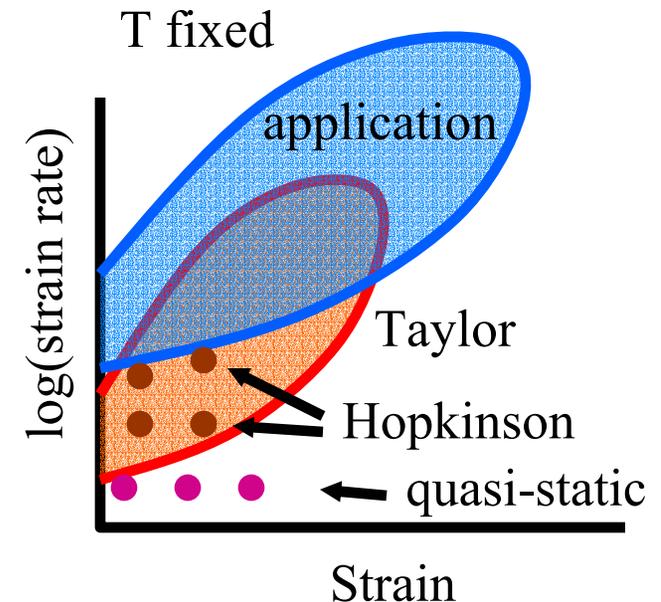
- Simulation of Taylor impact test
 - ▶ cylinder: high-strength steel, HSLA100, 15-mm dia, 38-mm long, room temperature
 - ▶ impact velocity = 247 m/s
 - ▶ CASH - Lagrangian code (X-7)
 - ▶ Zerilli-Armstrong model for rate-dependent strength and plasticity
 - ▶ ignore anisotropy, fracture effects
- Effective total strain exceeds 100%
- Temperature rises more than 400 °C



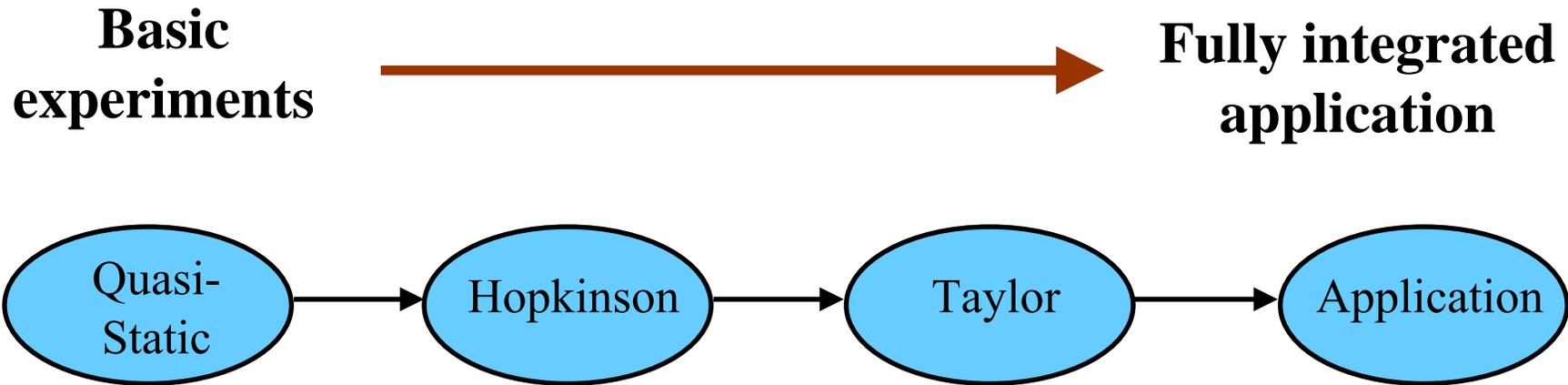
HSLA 100
247 m/s, 298°K

Hierarchy of experiments - plasticity

- Basic characterization experiments – measure stress-strain relationship at specific strain and strain rate
 - ▶ quasi-static – low strain rates
 - ▶ Hopkinson bar – medium strain rates
- Partially integrated expts. - Taylor test
 - ▶ covers range of strain rates
 - ▶ extends range of physical conditions
- Full integrated experiments
 - ▶ mimic application as much as possible
 - ▶ may involve extrapolation of operating range; introduces additional uncertainty
 - ▶ integrated expts. can help reduce model uncertainties in their operating range; may expose model deficiencies



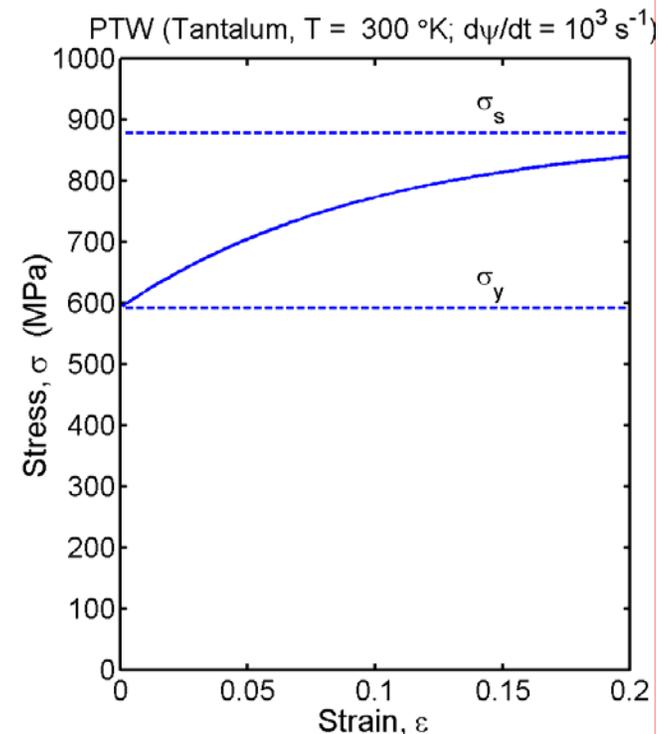
Analysis of hierarchy of experiments



- Series of experiments to determine plastic behavior of a metal
- Information flow shown for analysis sequence
- Bayesian calibration –
 - ▶ analysis of each experiment updates model parameters and their uncertainties, consistent with previous experiments
 - ▶ information about models accumulates throughout process

PTW model for plastic deformation

- Preston-Tonks-Wallace model describes plastic behavior of metals
 - ▶ provides stress σ (or s) as function of plastic strain ε_p for wide range of strain rate and temperature
 - ▶ nonlinear, analytic formulation
- 7 parameters (for low strain rates) plus material-specific constants
- PTW model based on dislocation mechanics model
 - ▶ does not include effects of anisotropy or material history



The model and parameter inference

- We write the model as

$$\mathbf{y} = \mathbf{y}(\mathbf{x}, \mathbf{a})$$

- ▶ where \mathbf{y} is a vector of physical quantities, which is modeled as a function of the independent variables vector \mathbf{x} and \mathbf{a} represents the model parameters vector
- In inference, the aim is to determine:
 - ▶ the parameters \mathbf{a} from a set of n measurements d_i of \mathbf{y} under specified conditions x_i
 - ▶ and the uncertainties in the parameter values
- This process is called parameter inference, model fitting (or regression), however, uncertainty analysis is often not done, only parameters estimated

Likelihood analysis

- When the errors in each measurement are Gaussian distributed and independent, likelihood is related to chi squared:

$$p(\mathbf{d} | \mathbf{a}) \propto \exp(-\frac{1}{2} \chi^2) = \exp \left\{ -\frac{1}{2} \sum_i \left[\frac{[d_i - y_i(\mathbf{a})]^2}{\sigma_i^2} \right] \right\}$$

- χ^2 is quadratic in the parameters \mathbf{a}

$$\chi^2(\mathbf{a}) = \frac{1}{2} (\mathbf{a} - \hat{\mathbf{a}})^T \mathbf{K} (\mathbf{a} - \hat{\mathbf{a}}) + \chi^2(\hat{\mathbf{a}})$$

- ▶ where $\hat{\mathbf{a}}$ is the parameter vector at minimum χ^2 and \mathbf{K} is the curvature matrix (aka the *Hessian*)

- The covariance matrix for the uncertainties in the estimated parameters is

$$\text{cov}(\mathbf{a}) \equiv \left\langle (\mathbf{a} - \hat{\mathbf{a}})(\mathbf{a} - \hat{\mathbf{a}})^T \right\rangle \equiv \mathbf{C} = 2\mathbf{K}^{-1}$$

Characterization of chi-squared

- Expand vector \mathbf{y} around \mathbf{y}^0 :

$$y_i = y_i(x_i, \mathbf{a}) = y_i^0 + \sum_j \left. \frac{\partial y_i}{\partial a_j} \right|_{\mathbf{a}^0} (a_j - a_j^0) + \dots$$

- The derivative matrix is called the *Jacobian*, \mathbf{J}
- Estimated parameters $\hat{\mathbf{a}}$ minimize χ^2 (MAP estimate)
- As a function of \mathbf{a} , χ^2 is quadratic in $\mathbf{a} - \hat{\mathbf{a}}$

$$\chi^2(\mathbf{a}) = \frac{1}{2} (\mathbf{a} - \hat{\mathbf{a}})^T \mathbf{K} (\mathbf{a} - \hat{\mathbf{a}}) + \chi^2(\hat{\mathbf{a}})$$

- ▶ where \mathbf{K} is the curvature matrix (aka the *Hessian*);

$$[\mathbf{K}]_{jk} = \left. \frac{\partial^2 \chi^2}{\partial a_j \partial a_k} \right|_{\hat{\mathbf{a}}} ; \quad \mathbf{K} = \mathbf{J} \mathbf{\Lambda} \mathbf{J}^T ; \quad \mathbf{\Lambda} = \text{diag}(\sigma_1^{-2}, \sigma_2^{-2}, \sigma_3^{-2}, \dots)$$

- Jacobian useful for finding min. χ^2 , i.e., optimization

Advanced analysis

- Analysis of multiple data sets
 - ▶ To combine the data from multiple, independent data sets into a single analysis, the combined chi squared is

$$\chi_{all}^2 = \sum_k \chi_k^2$$

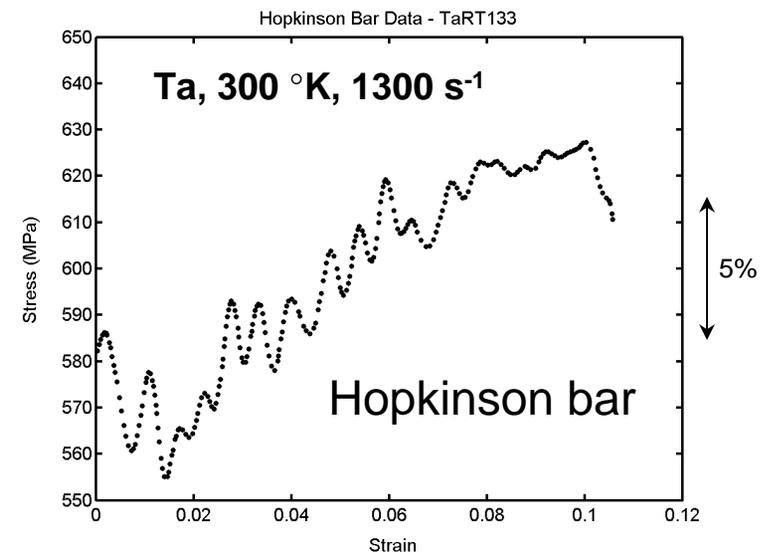
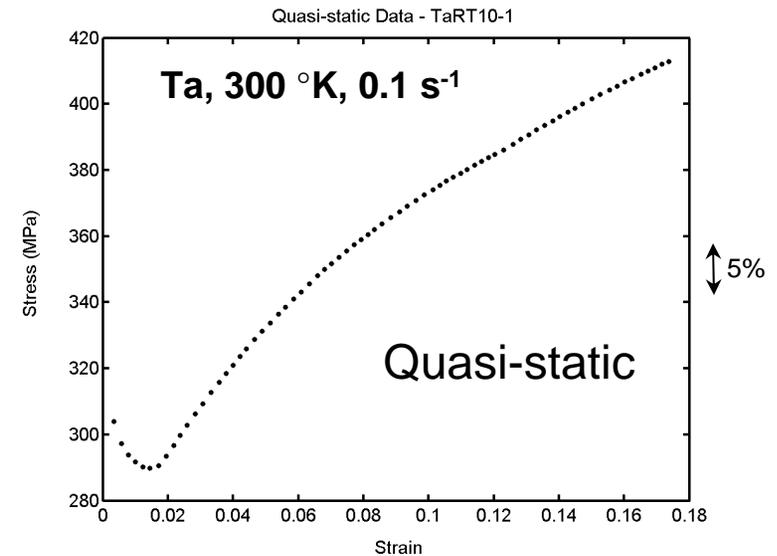
- ▶ where $p(\mathbf{d}_k | \mathbf{a}, I)$ is likelihood from k th data set
- Include Gaussian priors through Bayes theorem

$$p(\mathbf{a} | \mathbf{d}, I) \propto p(\mathbf{d} | \mathbf{a}, I) p(\mathbf{a} | I)$$

- ▶ For a Gaussian prior on a parameter \mathbf{a}
$$-\log p(\mathbf{a} | \mathbf{d}, I) = \varphi(\mathbf{a}) = \frac{1}{2} \chi^2 + \frac{(\mathbf{a} - \tilde{\mathbf{a}})^2}{2\sigma_a^2}$$
 - ▶ where $\tilde{\mathbf{a}}$ is the default value for \mathbf{a} and σ_a^2 is assumed variance

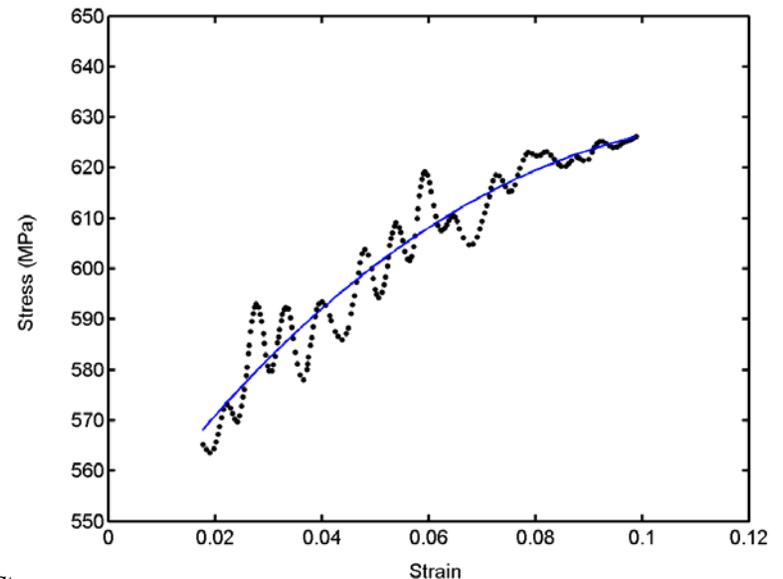
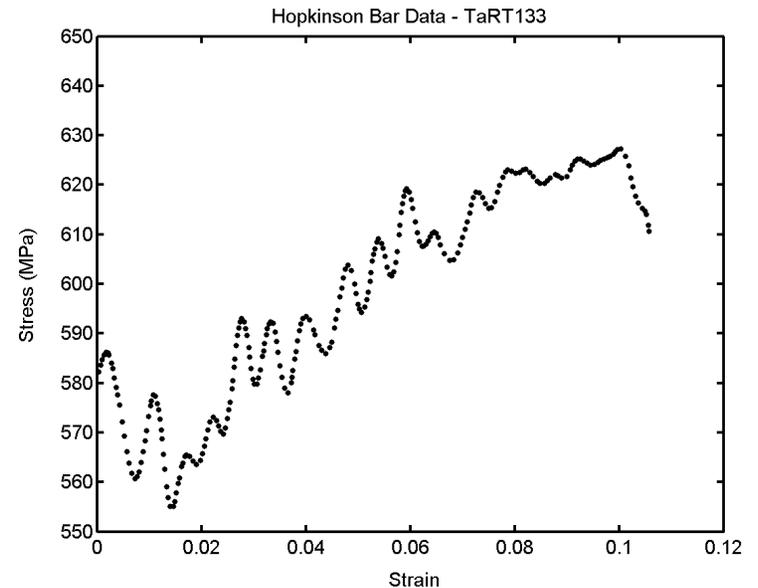
Material-characterization experiments

- Data from **quasi-static** compression experiments tend to be of high quality
 - ▶ rms 'noise' $\approx 0.1\%$
 - ▶ thin data set to limit undue influence in likelihood
- Data from **Hopkinson-bar** experiments tend to be of medium quality
 - ▶ rms 'noise' $\approx 1\%$
- Observe artifacts in the data
 - ▶ arise from reflected shocks
 - ▶ need to account for these



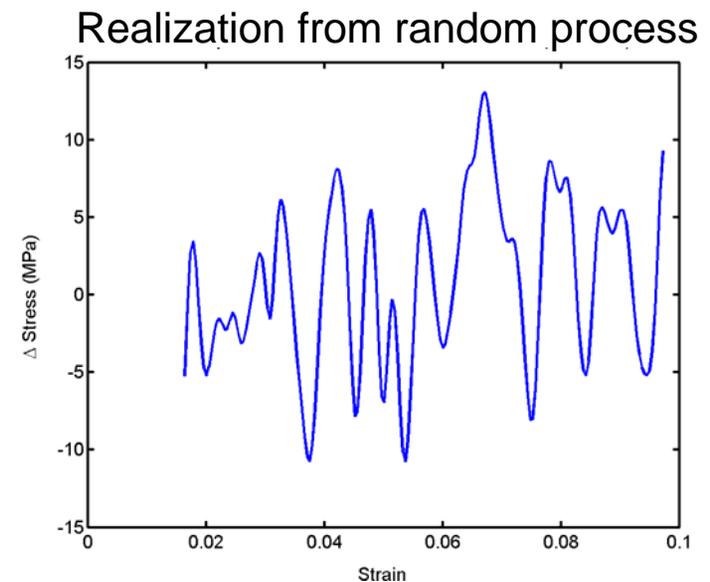
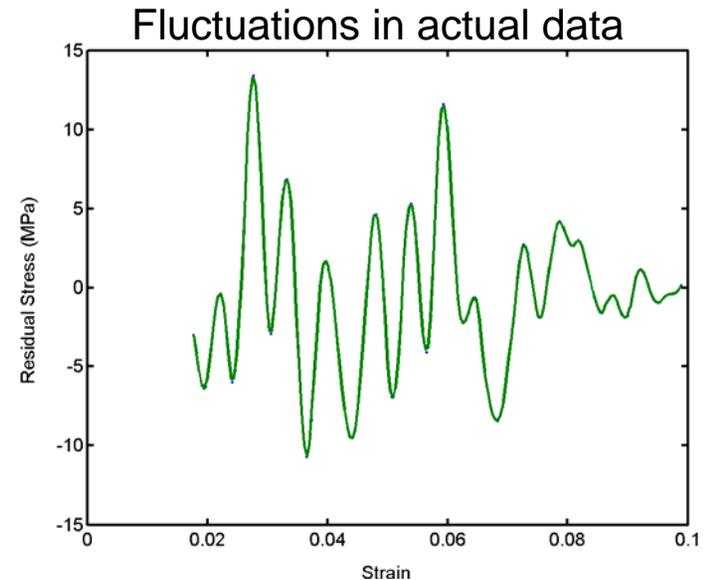
Hopkinson bar measurements

- Hopkinson-bar data are degraded by oscillations, caused by reflected shocks and bar oscillations
- Treat these fluctuations as a random process with a high degree of correlation from point to point
- Subtract low-order polynomial from data to get fluctuations from smooth dependence



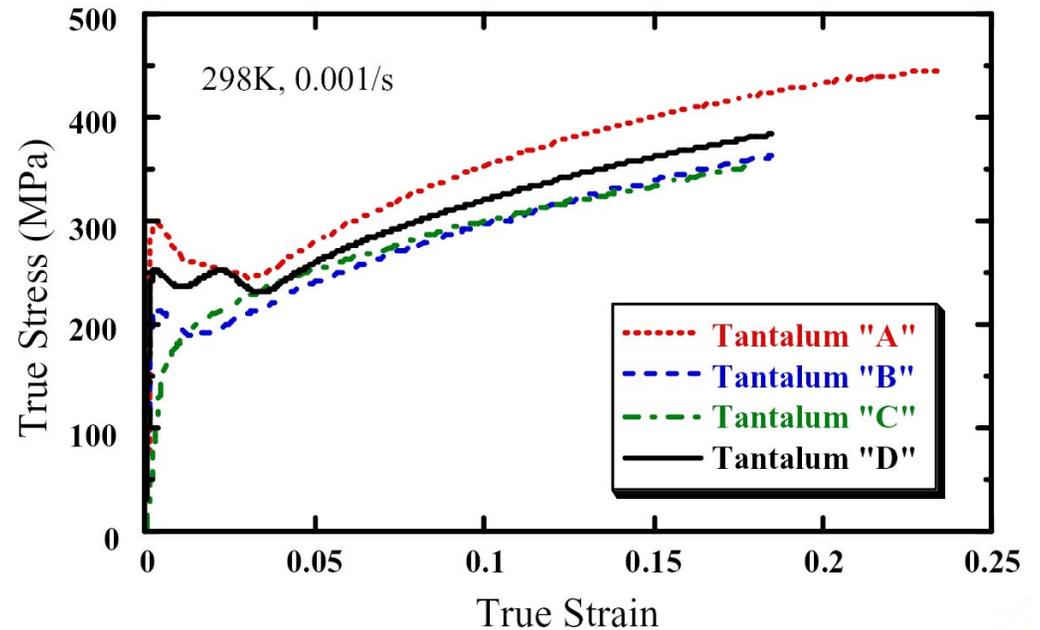
Hopkinson bar measurements

- Treat Hop-bar fluctuations as a correlated Gaussian process; covariance given by
$$\text{cov}(\mathbf{y}, \mathbf{y}') \propto \exp \left\{ - \left[\frac{\mathbf{x} - \mathbf{x}'}{\lambda} \right]^p \right\}$$
 - ▶ where x is independent variable, strain
 - ▶ determine correlation length λ and exponent p from data
 - ▶ $p \cong 2$; $\lambda \cong 0.002$ (about 4 samples)
- Realization of random process shows behavior similar to data fluctuations
- Thin data set to avoid giving data undue weight in likelihood



Repeated experiments

- Repeated experiments
 - ▶ stability of apparatus
 - ▶ indication of random component of error
 - ▶ may or may not indicate systematic error
- Figure shows curves obtained from four samples taken from different lots
- Sample-to-sample rms dev. $\approx 8\%$
- Treat this variability as a **systematic uncertainty** common to each specimen
- Represents an uncertainty in initial state



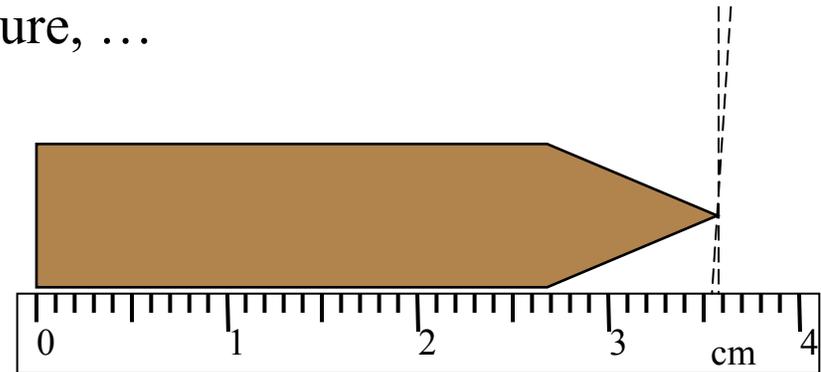
†data supplied by S-R Chen, MST-8

Types of uncertainties in measurements

- Two major types of errors
 - ▶ random error – different for each measurement
 - in repeated measurements, get different answer each time
 - often assumed to be statistically independent, but often aren't
 - ▶ systematic error – same for all measurements within a group
 - component of measurements that remains unchanged
 - for example, caused by error in calibration or zeroing
- Nomenclature varies
 - ▶ physics – random error and systematic error
 - ▶ statistics – random and bias
 - ▶ metrology standards (NIST, ASME, ISO) – random and systematic uncertainties (now)

Types of uncertainties in measurements

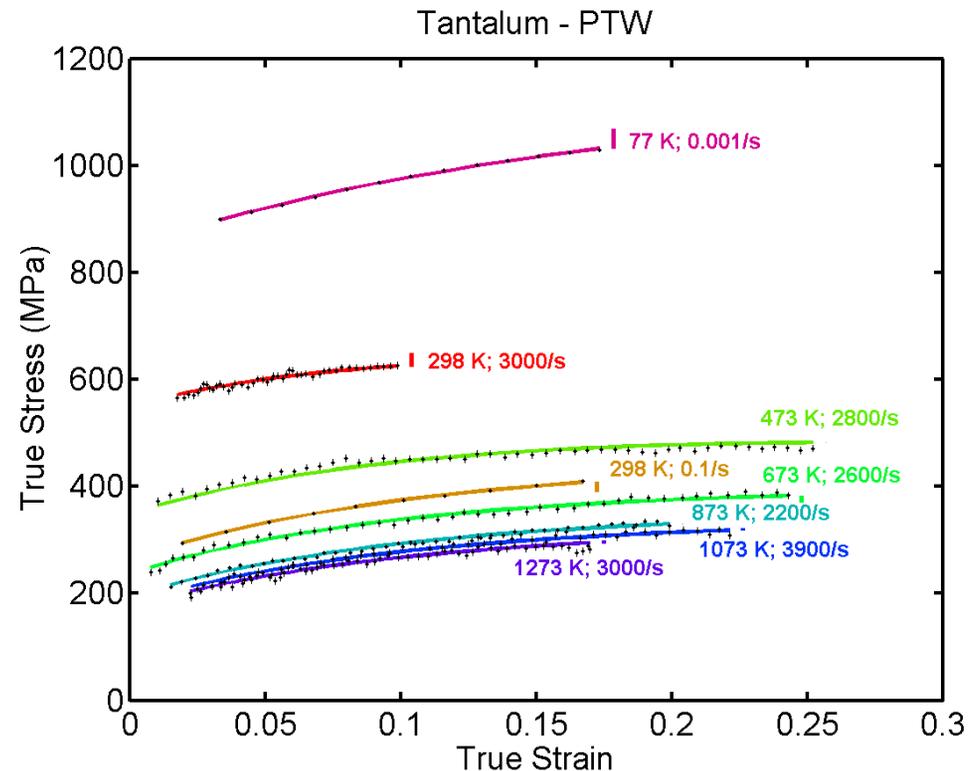
- Simple example – measurement of length of a pencil
 - ▶ random error
 - interpolation between ruler tick marks
 - ▶ systematic error
 - accuracy of ruler's calibration; manufacturing defect, temperature, ...
- Parallax in measurements
 - ▶ reading depends on how person lines up pencil tip
 - ▶ random or systematic error?
 - depends on whether measurements always made by same person in the same way or made by different people



Fit PTW model to measurements

Analysis of quasi-static and Hopkinson bar measurements[†]

- PTW model for rate- and temperature-dependent plasticity
- Parameters estimated from Hopkinson bar measurements and quasi-static tests
- Full uncertainty analysis – **include 3% systematic uncertainty** in offset of each data set (8 + 7 parms)
- ~ 6 iter., ~ 100 func. evals.



PTW curves include adiabatic heating effect for high strain rates

[†]data supplied by S-R Chen, MST-8

PTW parameters and their uncertainties

Parameters +/- rms error:

$$y_0 = 0.0123 \pm 0.0006$$

$$y_\infty = 0.00164 \pm 0.00004$$

$$s_0 = 0.0164 \pm 0.0007$$

$$s_\infty = 0.00308 \pm 0.00005$$

$$\kappa = 0.91 \pm 0.08$$

$$\gamma = (2.4 \pm 2.0) \times 10^{-6}$$

$$\theta = 0.0145 \pm 0.0002$$

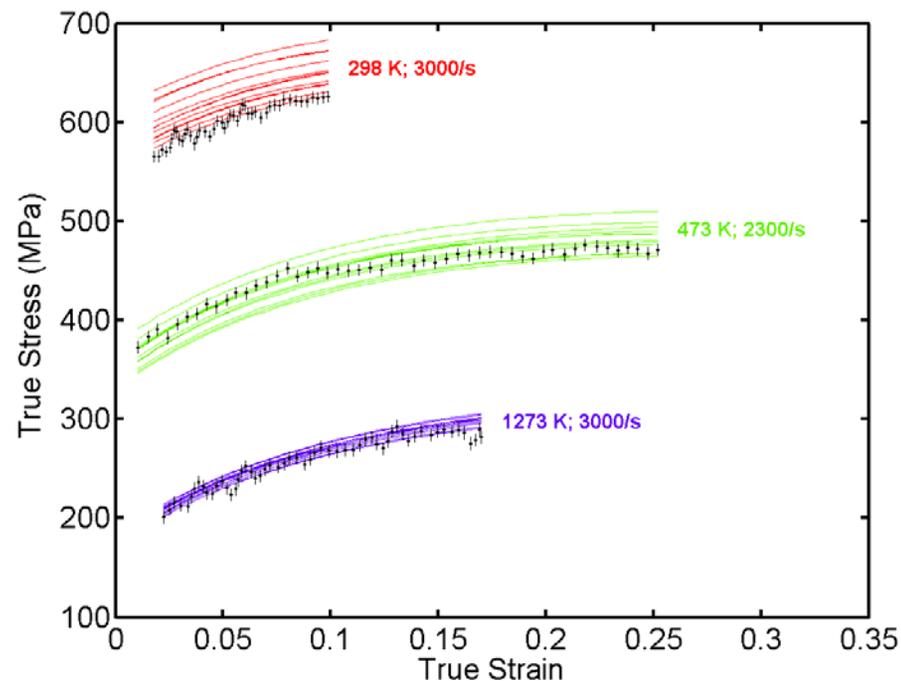
Minimum chi-squared fit yields estimated PTW parms. and rms errors, including correlation coefficients, which are crucially important!

Correlation coefficients

	y_0	y_∞	s_0	s_∞	κ	γ	θ
y_0	1	0.186	0.988	0.400	0.687	-0.464	-0.182
y_∞	0.186	1	0.208	0.913	0.142	0.022	-0.140
s_0	0.988	0.208	1	0.432	0.713	-0.496	-0.299
s_∞	0.400	0.913	0.432	1	0.443	-0.263	-0.257
κ	0.687	0.142	0.713	0.443	1	-0.935	-0.119
γ	-0.464	0.022	-0.496	-0.263	-0.935	1	0.087
θ	-0.182	-0.140	-0.299	-0.257	-0.119	0.087	1

Monte Carlo sampling of PTW uncertainty

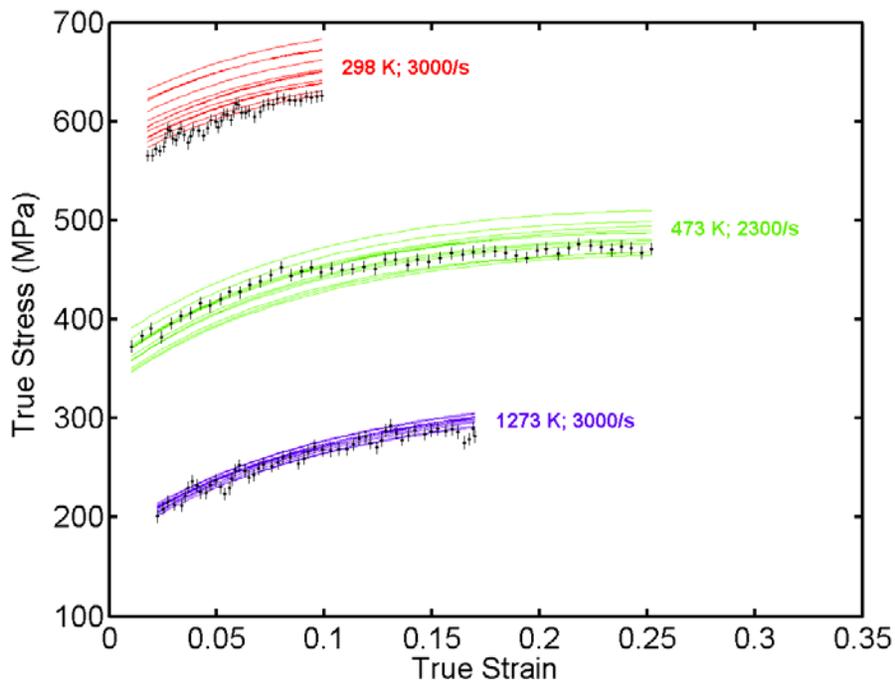
- Use Monte Carlo technique - draw random samples from complete uncertainty distribution for PTW parameters
- Display stress-strain curve for each parameter set (at three temps)
- Conclude that fit faithfully represents data and their errors
- This procedure confirms the analysis and model



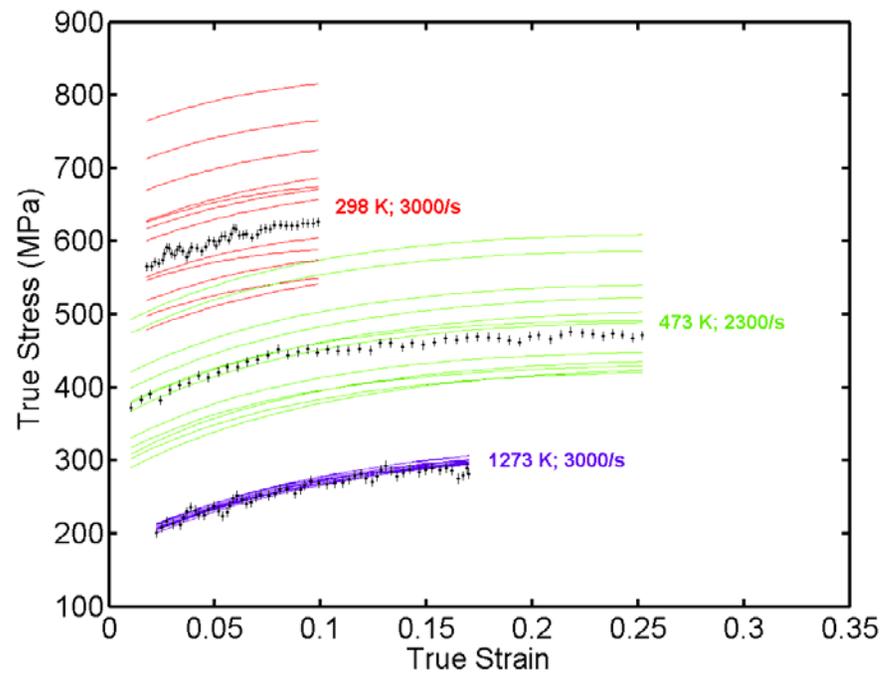
Importance of including correlations

- Monte Carlo draws from uncertainty distribution, done correctly with full covariance matrix (left) and incorrectly (right), by neglecting off-diagonal terms in covariance matrix

MC with correlations



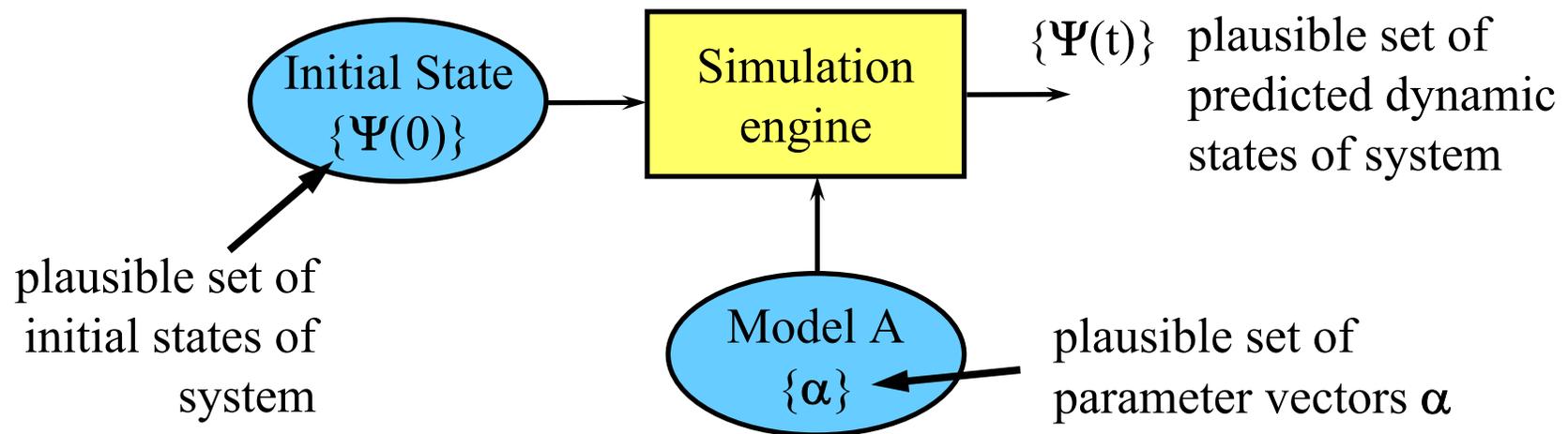
MC without correlations



Future work: Taylor impact experiment

- Next step in plan to validate PTW model is to proceed to next level of hierarchy of experiments
- Analyze data from Taylor impact experiments
 - ▶ need to use simulation code
 - ▶ use posterior distribution from foregoing analysis as prior
 - ▶ determine posterior distribution for Taylor data
 - ▶ check consistency with Taylor data
 - ▶ check consistency with prior
 - ▶ resolve discrepancies or cope with model deficiencies
- Then proceed to analysis of more complex experiments, which extend the operating range, e.g., flyer -impact experiments

Plausible simulation predictions (forward)



- Generate plausible predictions for known uncertainties in parameters and initial conditions
- Monte Carlo method
 - ▶ run simulation code for each random draw from pdf for α , $p(\alpha | \cdot)$, and initial state, $p(\Psi(0) | \cdot)$
 - ▶ simulation outputs represent plausible set of predictions, $\{\Psi(t)\}$
 - ▶ advanced sampling methods useful to reduce number of calcs needed
 - Latin Hypercube, Centroidal Voronoi Tessellations, etc.

Summary

- Physics simulations codes
 - ▶ employ hierarchy of experiments, from basic to fully integrated
 - ▶ role of Bayesian analysis - improve knowledge of models with each new experiment
- Analysis of experimental data to infer parameters of Preston-Tonks-Wallace plasticity model for tantalum
 - ▶ characterize uncertainties in measurement data
 - ▶ estimate PTW parameters and their uncertainties
 - ▶ demonstrate importance of including correlations

Bibliography

- ▶ “Uncertainty quantification of simulation codes based on experimental data,” K. M. Hanson and F. M. Hemez, *Proc. AIAA Aerospace Conf.* (2003)
- ▶ “A framework for assessing confidence in simulation codes,” K. M. Hanson and F. M. Hemez, *Experimental Techniques* **25**, pp. 50-55 (2001); application of uncertainty quantification to simulation codes with Taylor test as example
- ▶ “A framework for assessing uncertainties in simulation predictions,” K. M. Hanson, *Physica D* **133**, pp. 179-188 (2000); an integrated approach to determining uncertainties in physics modules and their effect on predictions
- ▶ “Inversion based on complex simulations,” K. M. Hanson, *Maximum Entropy and Bayesian Methods*, pp. 121-135 (Kluwer Academic, 1998); describes adjoint differentiation and its usefulness in simulation physics
- ▶ “Uncertainty assessment for reconstructions based on deformable models,” K. M. Hanson et al., *Int. J. Imaging Syst. Technol.* **8**, pp. 506-512 (1997); use of MCMC to sample posterior

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